

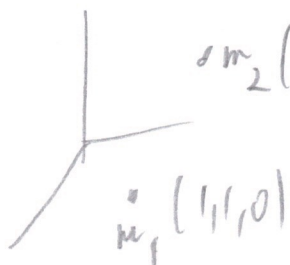
What is I ?

$$I \equiv \sum m_i r_i^2 = ?$$

mass points m_1 at \underline{r}_1 , m_2 at \underline{r}_2 ...

just add them up

e.g.



$m_2(2, 5, 3)$

$$I = m_1(1^2 + 1^2) + m_2(2^2 + 5^2) \dots$$

continuous bodies $m_i = \rho(\underline{r}_i) dV$ $\rho = \text{density}$

$$M = \sum m_i = \sum \rho(\underline{r}_i) dV \rightarrow \int dV \rho(\underline{r})$$

$$I = \sum m_i r_i^2 = \sum \rho(\underline{r}_i) dV r_i^2 \rightarrow \int dV \rho(\underline{r}) r^2$$

which is a calculus problem

Ex 1: rod rotating about an end in a plane



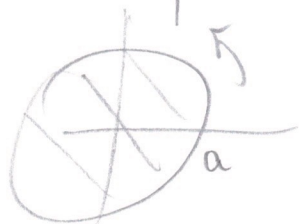
$s = \text{coordinate along rod}$

$\lambda = \text{mass/length}$

$$I = \int_0^l (\lambda ds) s^2 = \lambda l^3 / 3$$

$$\rightarrow \frac{1}{3} M l^2, \quad M = \lambda l$$

Ex 2: cylinder rotating about its axis



$$I = \int d^3r \rho r^2$$

$$\rightarrow \int_0^{2\pi} d\phi \int_0^a \sigma d\sigma \int_0^L dz \cdot \rho \sigma^2$$

$$= 2\pi \cdot \frac{a^4}{4} \cdot L \cdot \rho = \frac{1}{2} (\rho \pi a^2 L) a^2 = \frac{1}{2} M a^2$$

Ex 3 sphere rotating about a diameter



$$I = \int_0^{2\pi} d\varphi \int_0^\pi \sin\theta d\theta \int_0^a r^2 dr \cdot \rho \cdot \underbrace{(x^2 + y^2)}_{r^2 \sin^2\theta}$$

$$= 2\pi \cdot \frac{4}{3} \cdot \frac{a^5}{5} \cdot \rho = \frac{2}{5} \left(\frac{4}{3} \pi a^3 \rho \right) \cdot a^2$$

$$= \frac{2}{5} M a^2$$

What about a cylinder rotating about a point on circumference?



very messy calculus problem

Instead use Parallel Axis Theorem:

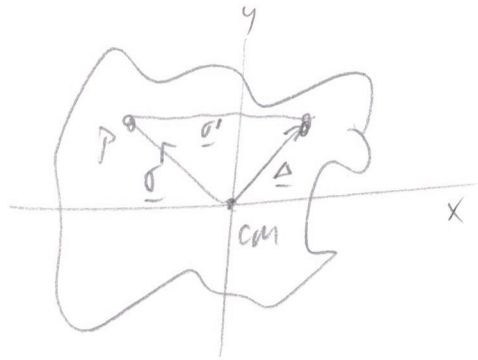
I_0 = moment of inertia about CM

I_A = " " about // axis displaced by Δ in plane

$$\text{then } I_A = I_0 + M \Delta^2$$

proof: take CM at origin, \hat{z} = rotation axis

at one z



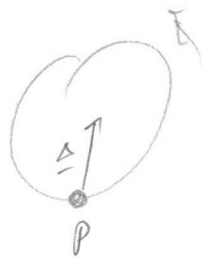
$$I_{cm} = \int d^3r \rho \sigma^2$$

$$R_{cm} = \frac{1}{M} \int d^3r \rho (\sigma_x \sigma_{y,z}) = 0$$

$$I_a = \int d^3r \rho \sigma'^2 = \int d^3r \rho (\sigma - \Delta)^2$$

$$= \underbrace{\int d^3r \rho \sigma^2}_{I_0} - 2\Delta \cdot \underbrace{\int d^3r \rho \sigma}_0 + \underbrace{\Delta^2}_{M} \int d^3r \rho$$

So for

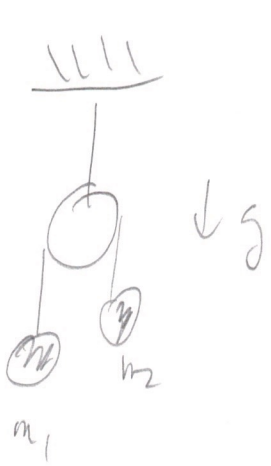


$$I_P = I_{cm} + M \Delta^2$$

$$= \frac{1}{2} M a^2 + M \cdot a^2 = \frac{3}{2} M a^2$$

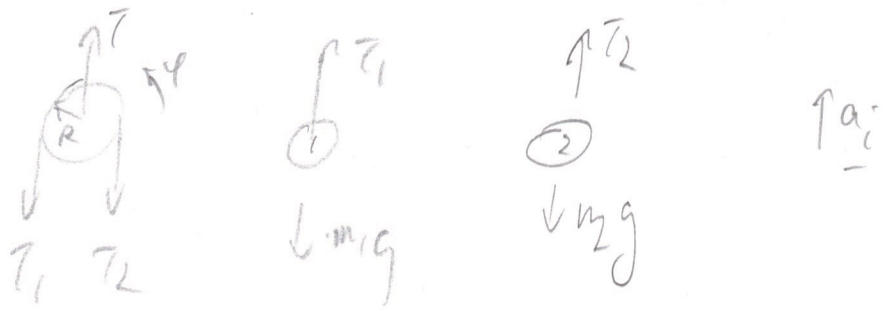
I_Δ is bigger because the mass is further from the rotation axis.

Example - Atwood's machine



massless, unstretchable string
 ("??") frictionless pulley
 no slipping

vertical force balance



IF $I=0$

$$m_1 a_1 = T_1 - m_1 g$$

$$m_2 a_2 = T_2 - m_2 g$$

torque balance on pulley

$$(T_1 - T_2) \cdot R = I \ddot{\phi} \rightarrow 0$$

$$\rightarrow T_1 = T_2$$

unstretchable $\rightarrow a_1 = -a_2 \rightarrow$

$$m_1 a_1 = T - m_1 g$$

$$-m_2 a_1 = T - m_2 g$$

$$a_1 = \frac{m_2 - m_1}{m_2 + m_1} g$$

IF $I \neq 0$

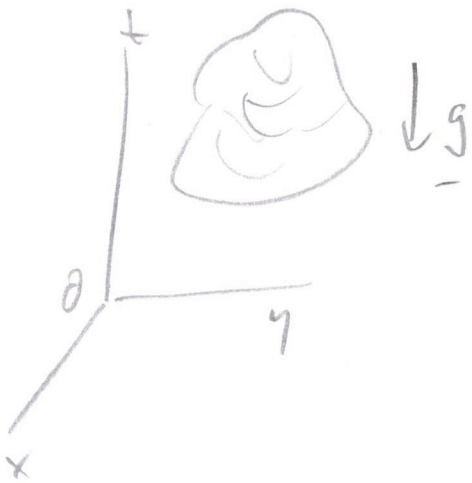
$$R \ddot{\phi} = -a_1, \quad T_1 - T_2 = -\frac{I}{R^2} \cdot a_1 \xrightarrow{\text{cyl.}} -\frac{1}{2} M a_1$$

{ this uses $\frac{dL}{dt} = \tau$, $L = \frac{1}{2} I \dot{\phi}^2$ wrt fixed center of pulley. }

$$\dots a_1 = \frac{m_2 - m_1}{m_2 + m_1 + \frac{1}{2} M} g$$

General remark:

gravitational forces + torques "act out the CM"



$$\underline{F}_{\text{grav}} = \sum_i m_i \underline{g} = M \underline{g}$$

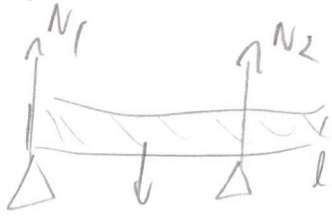
$$\underline{\Gamma}_{\text{grav}} = \sum_i \underline{r}_i \times (m_i \underline{g})$$

$$= \left(\sum_i m_i \underline{r}_i \right) \times \underline{g}$$

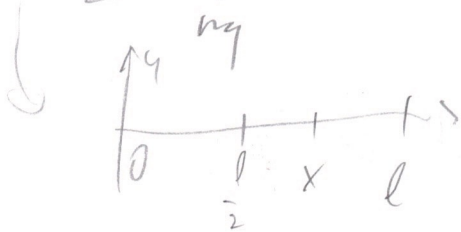
$$= \underline{R}_{\text{cm}} \times M \underline{g}$$

The shape of the object enters via \underline{I} .

Example: solid bar, supported at 2 points: 0 + x



force balance: $N_1 + N_2 = mg$



if $\frac{l}{2} < x < l$: $N_1 + N_2 = mg$

mom. about supports

$$\begin{cases} \Gamma_0 = -mg \cdot \frac{l}{2} + N_2 x = 0 \\ \Gamma_x = mg \left(x - \frac{l}{2}\right) - N_1 x = 0 \end{cases}$$

so $N_1 = mg \left(1 - \frac{l}{2x}\right)$, $N_2 = mg \cdot \frac{l}{2x}$; $N_1 + N_2 = mg$ ✓

Torque about some other point y:

$$\begin{aligned} \Gamma_y &= -N_1 \cdot y + mg \cdot \left(y - \frac{l}{2}\right) + N_2(x - y) \\ &= -mg \left(y - \frac{l}{2}\right) + mg \left(y - \frac{l}{2}\right) + mg \frac{l}{2} - mg \frac{y}{2} = 0 \end{aligned}$$

What if $0 < x < \frac{l}{2}$?

$$\Gamma_x = -N_1 x - mg \left(\frac{l}{2} - x\right) < 0 : \text{not stable.}$$

Remove support 2; $N_1 = ?$

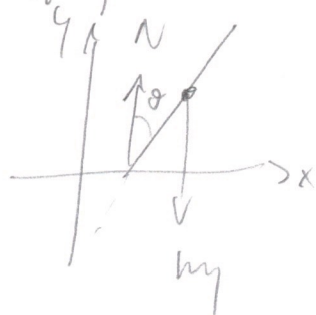
about 1

$$\Gamma_1 = I_1 \alpha = -mg \frac{l}{2} \quad \text{so } \alpha = -\frac{3g}{2l} \rightarrow a_{cm} = \frac{l}{3} \alpha = -\frac{3g}{4}$$

$$I_1 = \frac{1}{3} m l^2$$

$$N_1 - mg = ma \rightarrow N_1 = \frac{mg}{4}$$

Example: pencil tipping over on a frictionless table



$\theta = \text{tip angle}$

$(x, y) = \text{CM coordinates}$

$$m\ddot{x} = 0 \quad \text{so} \quad \dot{x} = \text{const} \rightarrow 0 \quad \text{if starts at rest.}$$

$$m\dot{y} = N - mg$$

$$I_{\text{cm}} \ddot{\theta} = \tau_{\text{cm}} \quad \text{or} \quad I_{\text{cm}} \ddot{\theta} = +Nl \sin(\pi - \theta) = Nl \sin \theta$$

geometry: $y = l \cos \theta \quad \text{so} \quad \dot{y} = -l \sin \theta \dot{\theta}$
 $\ddot{y} = -l (\cos \theta \dot{\theta}^2 + \ddot{\theta} \sin \theta)$

|| axis th: $I_{\text{cm}} = \frac{1}{3} ml^2 - m(l/2)^2 = \frac{1}{12} ml^2$
 I_{tip}

combine

$$I_{\text{cm}} \ddot{\theta} = (m\dot{y} + m\ddot{y}) l \sin \theta$$

$$= ml \sin \theta (g - l \dot{\theta}^2 \cos \theta - l \ddot{\theta} \sin \theta)$$

$$\ddot{\theta} = \sin \theta (g - \dot{\theta}^2 l \cos \theta) / \left(\frac{1}{12} + \sin^2 \theta \right) l$$

Add friction:

$$m\ddot{x} = \mu_s N \quad (+ \text{ to prevent sliding to left})$$

$$m\dot{y} = N - mg$$

$$I_{\text{cm}} \ddot{\theta} = Nl \sin \theta - \mu_s N l \cos \theta$$

etc.

For small θ : $\ddot{\theta} \approx \frac{12g}{l} \sin \theta \leftarrow \dots$: unstable

Subslety: the derivation of $\underline{\dot{L}} = \underline{\dot{T}}$ assumed that $\underline{L} + \underline{T}$ were taken with some fixed point in space

In Atwood problem + 2nd method above this is true, but in 1st method used the CM which moves (accelerates!)
 Is this OK? \uparrow + pencil problem

Take an arbitrary point $\underline{\xi}(t)$ to define $\underline{L} + \underline{T}$

$$\underline{L}_{\xi} = \sum_i (\underline{r}_i - \underline{\xi}) \times m_i (\underline{\dot{r}}_i - \underline{\dot{\xi}}) \quad \underline{r}_i \text{ relative to fixed pt.}$$

$$= \sum_i \underline{r}_i \times m_i \underline{\dot{r}}_i - \underline{\xi} \times M \underline{\dot{R}} - M \underline{R} \times \underline{\dot{\xi}} + M \underline{\xi} \times \underline{\dot{\xi}}$$

$\therefore \underline{L}$ depends on choice of origin

$$\frac{d}{dt} \underline{L}_{\xi} = \sum_i (\underline{r}_i - \underline{\xi}) \times m_i (\underline{\ddot{r}}_i - \underline{\ddot{\xi}})$$

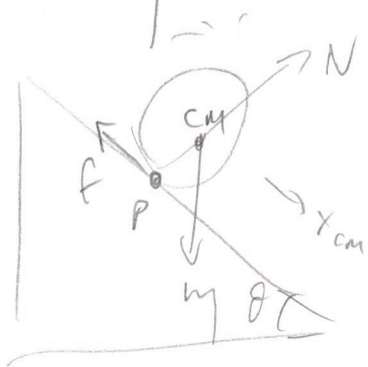
$$= \underbrace{\sum_i (\underline{r}_i - \underline{\xi}) \times \underline{F}_i}_{\underline{P}_{\xi}} - \underbrace{M \underline{R} \times \underline{\ddot{\xi}} + M \underline{\xi} \times \underline{\ddot{\xi}}}_{\text{extra terms}}$$

Extra terms $\rightarrow 0$ if (1) $\underline{\xi} = \underline{R} = \text{CM position}$

$$\underline{L}_{\text{cm}} = \underline{P}_{\text{cm}}, \quad \underline{L}_{\text{cm}} = \underline{L}_P - \underline{R} \times \underline{P}$$

or (2) $\underline{\ddot{\xi}} = 0 \rightarrow \underline{L}_{\xi} = \underline{P}_{\xi}$

Sphere rolling down an inclined plane: (3.55)



where f opposes motion at contact pt

pure rolling $x_{CM} = R\psi$

$\psi = \psi$ rolled angle

1. use $\underline{L}_{CM} = \underline{P}_{CM}$: $I_{CM} \ddot{\psi} = I_{CM} (-a_{CM}/R) = fR$

$$ma_{CM} = mg \sin \theta - f$$

eliminate f

$$(-ma_{CM} + mg \sin \theta) R = I_{CM} a_{CM} / R$$

$$a_{CM} = \frac{mg \sin \theta R}{mR + I_{CM}/R} = \frac{mg R^2 \sin \theta}{I_{CM} + mR^2}$$

2. use $\underline{L}_P = \underline{P}_P$: $I_P (a_{CM}/R) = mg R \sin(\pi - \theta)$
 $I_{CM} + mR^2$ $= \sin \theta$
 : see fig

If sphere placed at rest - friction holds contact point

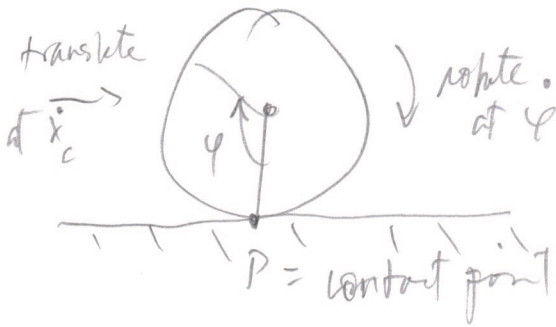
\rightarrow rotates

If thrown down - contact point slides at first

\rightarrow (later)

Rolling, sliding & slipping

ball (sphere or cyl.) moving across a plane surface



$x(t)$ = CM position

$\varphi(t)$ = angle rotated through at t

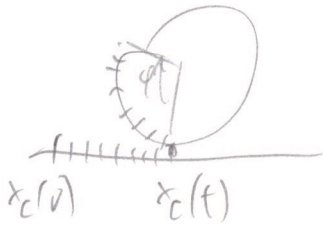
velocity of P relative to CM is $-R\dot{\varphi}$

so $\dot{x}_p = \dot{x}_c - R\dot{\varphi}$

pure sliding: while ball moves at \dot{x}_c , $\dot{\varphi} = 0$, $\dot{x}_p = \dot{x}_c$

pure rolling: $\dot{x}_p = 0$ $\dot{x}_c = R\dot{\varphi}$

(Other argument:



horizontal disp = \dot{x}_c at surface disp = $R\dot{\varphi}$ at these are =

intermediate case "slipping"

$\dot{x}_p > 0$ $\dot{x}_c > R\dot{\varphi} > 0$

friction: always opposes motion \rightarrow opposite \dot{x}_p



$f_s = \mu_s N \hat{x}$

slipping/sliding

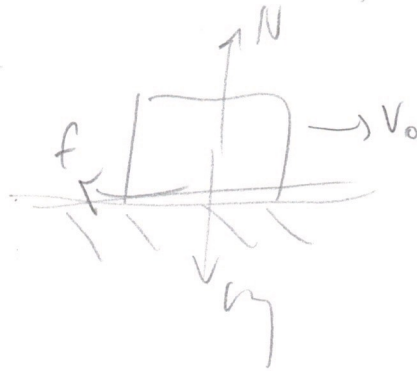


$f_k = -\mu_k N \hat{x}$

\rightarrow slipping tends to be transient

Transition from sliding to rolling

slider version



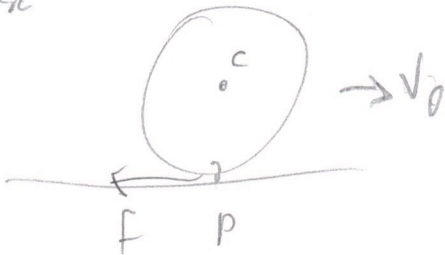
block set down at v_0

$$ma = -f = -\mu mg$$

$$v(t) = v_0 - \mu g t$$

stops $\rightarrow v = 0$ at $t = v_0 / \mu g$

disc



$$a = -\mu g \text{ again}$$

$$I \dot{\omega}_c = f R \rightarrow \dot{\omega}_c = -2\mu g / R$$

$$\omega_c(t) = -\frac{2\mu g}{R} t$$

$$v_{cm} = v_0 - \mu g t \text{ again}$$

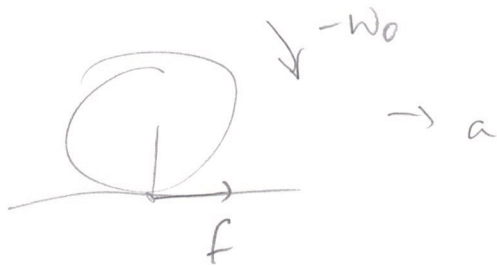
$$v_p = v_{cm} + R\omega = v_0 - 3\mu g t \rightarrow 0 \text{ at } t = v_0 / 3\mu g$$

at which point $v_{cm} = \frac{2}{3} v_0$

$$\omega = -2v_0 / 3R = -v_{cm} / R$$

and rolling starts.

Some Ring with initial angular velocity:



friction opposes relative motion at contact pt.

Start:

$$ma = f = \mu mg \quad \text{again}$$

$$I_C \dot{\omega}_C = fR \quad \rightarrow \quad \dot{\omega}_C = 2\mu g/R$$

After $v_{cm} = 0 + at = \mu g t$

$$V_P = v_{cm} + R\omega = \mu g t + R(-\omega_0 + 2\mu g t/R)$$

$$= 3\mu g t - R\omega_0 \quad \rightarrow \quad 0 \quad \text{at} \quad t = \frac{R\omega_0}{3\mu g}$$

where $v_{cm} = R\omega_0/3$

$$\omega_C = -\omega_0 + \frac{2\mu g}{R} \cdot \frac{R\omega_0}{3\mu g} = -\frac{1}{3}\omega_0$$

and $v_{cm} = -R\omega_C$ here.