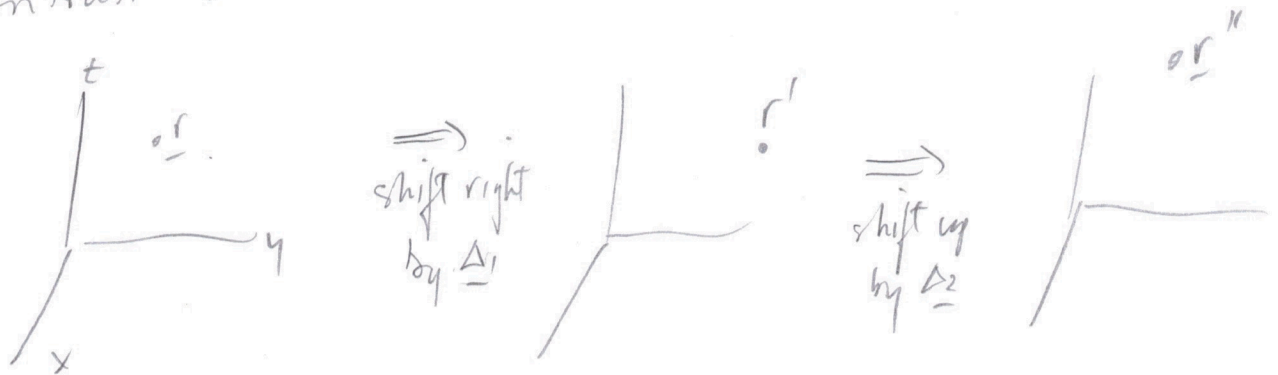


3d Rotations

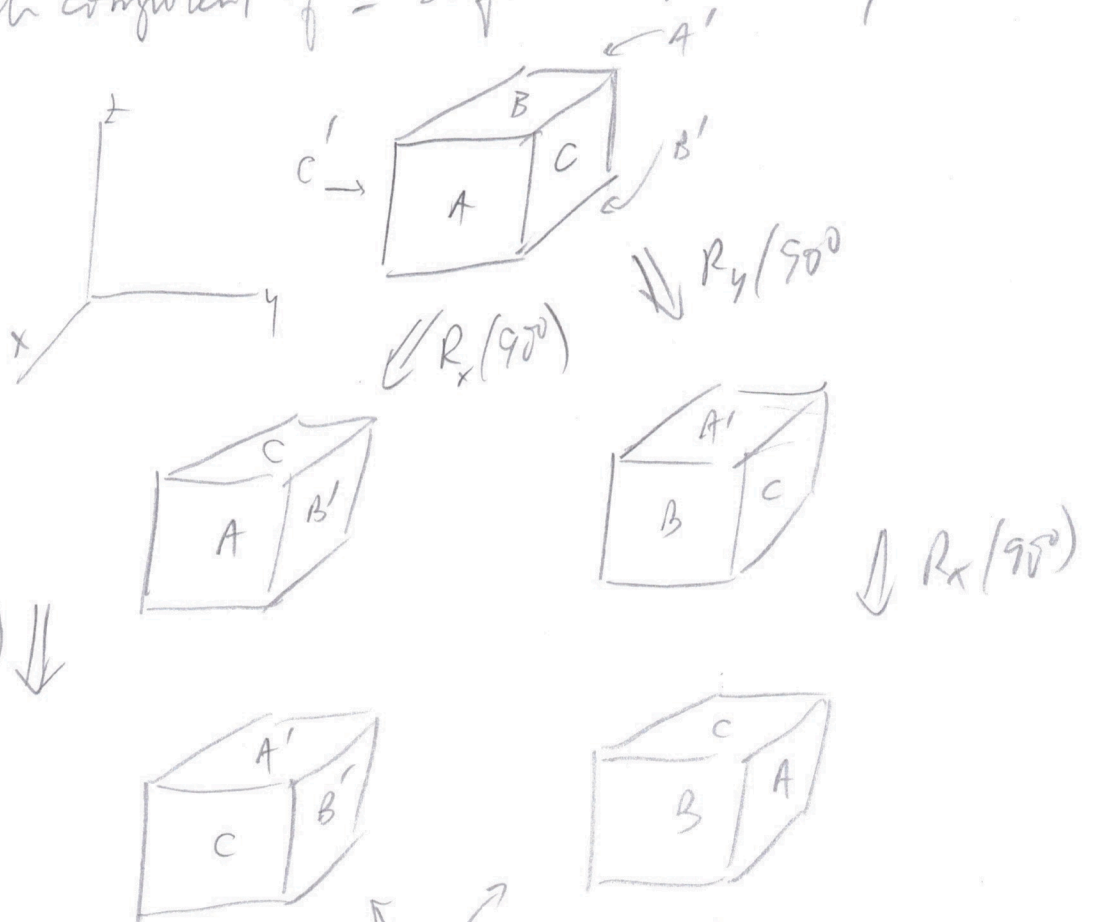
contrast to translations



$$\underline{r}' = \underline{r} + \underline{\Delta}_1 \quad \underline{r}'' = \underline{r}' + \underline{\Delta}_2 = \underline{r} + \underline{\Delta}_1 + \underline{\Delta}_2$$

→ { Same result if order reversed - translations "commute"
 Each component of \underline{r} shifts independently

rotation



not the same - rotations do not commute

Quantitative Argument:

write $\underline{r} = \begin{pmatrix} x \\ y \\ z \end{pmatrix}$ so $\underline{r} \rightarrow R \cdot \underline{r}$

where $R_z(\theta) = \begin{pmatrix} \cos\theta & -\sin\theta & 0 \\ \sin\theta & \cos\theta & 0 \\ 0 & 0 & 1 \end{pmatrix}$

used transformation

$R_y(\theta) = \begin{pmatrix} \cos\theta & 0 & \sin\theta \\ 0 & 1 & 0 \\ -\sin\theta & 0 & \cos\theta \end{pmatrix}$

$R_x(\theta) = \begin{pmatrix} 1 & 0 & 0 \\ 0 & \cos\theta & -\sin\theta \\ 0 & \sin\theta & \cos\theta \end{pmatrix}$

permute indices
 $x \rightarrow y \rightarrow z \rightarrow x \dots$
 $1 \rightarrow 2 \rightarrow 3 \rightarrow 1 \dots$

Then $\underline{r} \rightarrow R_y(\frac{\pi}{2}) \cdot (R_x(\frac{\pi}{2}) \cdot \underline{r}) = (R_y R_x) \cdot \underline{r}$ 1st case

$\underline{r} \rightarrow R_x(\frac{\pi}{2}) \cdot (R_y(\frac{\pi}{2}) \cdot \underline{r}) = (R_x R_y) \cdot \underline{r}$

and $R_y R_x \neq R_x R_y$: finite rotations don't commute

But infinitesimal ones do:

$\underline{r} \xrightarrow{\frac{d\theta_1}{dt}} \underline{r} + d\theta_1 \times \underline{r}$

$\xrightarrow{\frac{d\theta_2}{dt}} (\underline{r} + d\theta_1 \times \underline{r}) + d\theta_2 \times (\underline{r} + d\theta_1 \times \underline{r})$

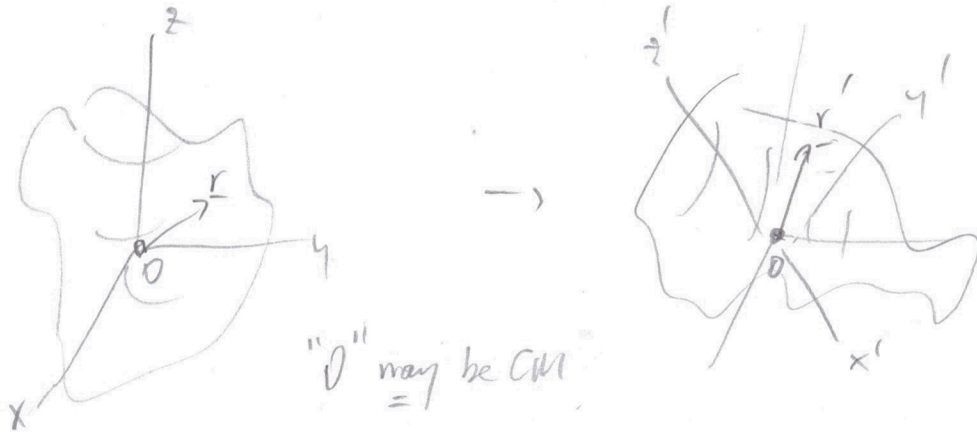
$= \underline{r} + (d\theta_1 + d\theta_2) \times \underline{r} + \underbrace{0/d\theta^2}$

independent of order

ignore

Finite rotations (for any axis):

Think of a coordinate system fixed in a solid body, which rotates about a fixed point "O".



old c-s $\underline{r} = x \hat{x} + y \hat{y} + z \hat{z}$ or $\underline{r} = \sum_{i=1}^3 r_i \hat{e}_i$

after rotation $\underline{r} \rightarrow \underline{r}' = x' \hat{x}' + y' \hat{y}' + z' \hat{z}'$
 also $= x \hat{x}' + y \hat{y}' + z \hat{z}'$

\hat{e}_i : $\underline{r}' =$ new components in old basis
 - old components in rotated basis

connection? $\hat{x} \cdot \underline{r}' = x' = (\hat{x} \cdot \hat{x}') x + (\hat{x} \cdot \hat{y}') y + (\hat{x} \cdot \hat{z}') z$
 $\hat{y} \cdot \underline{r}' = y' = (\hat{y} \cdot \hat{x}') x + \dots$

so new components are linear combinations of old ones.

Use 1-2-3 rotation $r_i' = a_{i1} r_1 + a_{i2} r_2 + a_{i3} r_3$ etc.

$a_{ij} \equiv \hat{e}_i \cdot \hat{e}_j' = \cos \theta_{ij}$ - "direction cosine"

$$r_i' = \sum_{j=1}^3 a_{ij} r_j$$

Matrix notation $\underline{r} = \begin{pmatrix} x \\ y \\ z \end{pmatrix}$ $\underline{A} = \begin{pmatrix} a_{11} & a_{12} & a_{13} \\ a_{21} & \dots & \dots \end{pmatrix}$

$$\rightarrow \underline{r}' = \underline{A} \cdot \underline{r}$$

Properties of \underline{A} : $a_{ij} = \text{real number}$, $|a_{ij}| \leq 1$

orthogonality - under rotation $\underline{r}^2 = \underline{r}'^2$

in matrix form, $\underline{r}^2 = r_1^2 + r_2^2 + r_3^2 = \begin{pmatrix} r_1 & r_2 & r_3 \end{pmatrix} \cdot \begin{pmatrix} r_1 \\ r_2 \\ r_3 \end{pmatrix}$
 $= \underline{r}^T \cdot \underline{r}$

$$\text{so } \underline{r}'^2 = \underline{r}'^T \underline{A}^T \underline{A} \underline{r} = \underline{r}^T \underline{r}$$

$$\uparrow r_i' = \sum_j A_{ij} r_j = \sum_j r_j (A^T)_{ji}$$

Holds for all \underline{r} so $\underline{A}^T \underline{A} = \underline{1} = \text{unit matrix} \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix}$

Also \underline{A}^{-1} exists because $\det(\underline{A}^T \underline{A}) = (\det \underline{A})^2 = \det \underline{1} = 1$
 (physically - can go back + forth for \underline{r} to \underline{r}')

$$\text{so } \underline{A}^T = (\underline{A}^T \underline{A}) \underline{A}^{-1} = \underline{1} \cdot \underline{A}^{-1} \text{ or } \underline{A}^T = \underline{A}^{-1}$$

$\rightarrow \underline{A} = \text{orthogonal matrix}$

Note: $\underline{r} = \text{any vector fixed in a rigid body}$

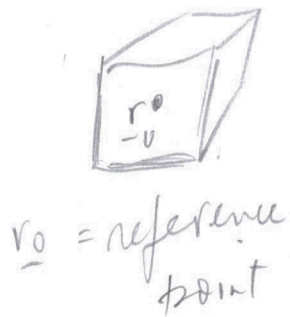
so $\underline{i}, \underline{j}, \underline{k}, \dots$ have the same transformation law.

Rotations always preserve lengths in rigid bodies, therefore
 always described by an orthogonal matrix

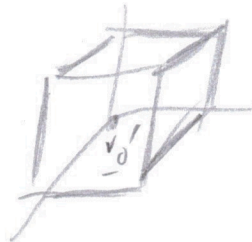
Converse - is any orth. matrix equivalent to a rotation
 by some angle about some axis?

Yes - Euler's Theorem (proof in Goldstein et al. book)

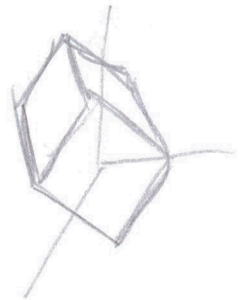
Characterization of finite motions:



translate r_0 to new position r_0'



rotate to final orientation

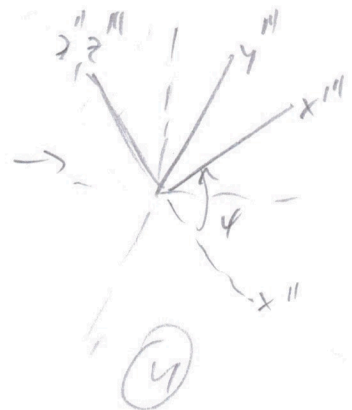
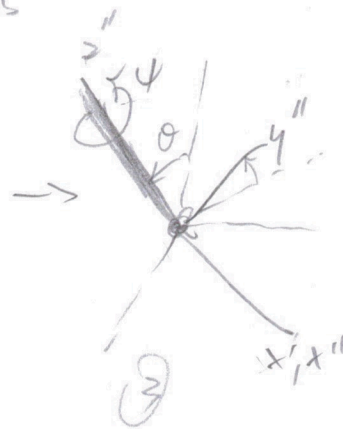
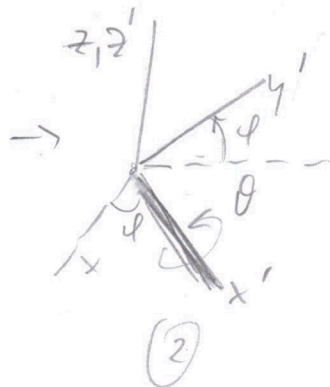
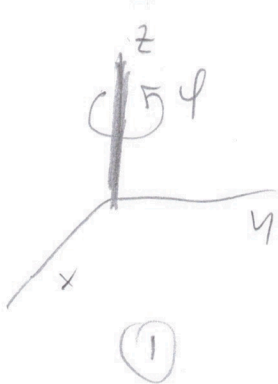


Usually not the actual motion.

How to specify orientation?

need 3 angles - 2 to give rotation axis (e.g. $\theta + \phi$)
 1 for rotation about the axis

convention - "Euler angles"



Dynamics

Focus on motion about point "0" fixed in a rigid body

→ masses m_i at $\underline{r}_0 + \underline{r}_i$; $\underline{\dot{r}}_i = \underline{\omega} \times \underline{r}_i$ since the motion w.r.t \underline{r}_0 is a rotation.

$$\begin{aligned} \underline{L} &= \sum_i (\underline{r}_0 + \underline{r}_i) \times m_i (\underline{\dot{r}}_0 + \underline{\dot{r}}_i) \\ &= \underline{r}_0 \times M \underline{\dot{r}}_0 + \underline{r}_0 \times \sum m_i \underline{\dot{r}}_i + \sum m_i \underline{r}_i \times \underline{\dot{r}}_0 + \sum m_i \underline{r}_i \times \underline{\dot{r}}_i \end{aligned}$$

$$\begin{aligned} T &= \sum_i \frac{1}{2} m_i (\underline{\dot{r}}_0 + \underline{\dot{r}}_i)^2 \\ &= \frac{1}{2} M \underline{\dot{r}}_0^2 + \underline{\dot{r}}_0 \cdot \sum m_i \underline{\dot{r}}_i + \frac{1}{2} \sum m_i \underline{\dot{r}}_i^2 \end{aligned}$$

In the coordinate system where \underline{r}_0 is fixed at the origin

$$\underline{L} \rightarrow \sum_i m_i \underline{r}_i \times (\underline{\omega} \times \underline{r}_i) = \sum_i m_i \left[\underline{\omega} r_i^2 - \underline{r}_i (\underline{\omega} \cdot \underline{r}_i) \right]$$

$$T \rightarrow \frac{1}{2} \sum m_i (\underline{\omega} \times \underline{r}_i)^2 = \sum_i \frac{1}{2} m_i \left[\underline{\omega}^2 r_i^2 - (\underline{\omega} \cdot \underline{r}_i)^2 \right]$$

(If 0 accelerates, get extra fictitious forces which affect the CM motion.)

Special case: $\underline{\omega} = \text{constant} = \omega \hat{z}$:

$$L_z = \omega \sum_i m_i (r_i^2 - z_i^2) = \omega \sum_i m_i (x_i^2 + y_i^2) = \omega I_{zz}$$

$$T = \frac{1}{2} \left(\sum_i m_i (x_i^2 + y_i^2) \right) \omega^2 = \frac{1}{2} I_{xx} \omega^2 \quad \left. \begin{array}{l} \text{studied} \\ \text{earlier} \end{array} \right\}$$

General case:

$$L_\alpha = \sum_i m_i \left[\omega_\alpha r_i^2 - r_{\alpha i} \left(\sum_\beta r_{\beta i} \omega_\beta \right) \right] \quad r_{\alpha i} - \alpha^{\text{th}} \text{ component of } \underline{r}_i$$

$\alpha = 1, 2, 3$

$$= \sum_\beta \left(\sum_i m_i (\delta_{\alpha\beta} r_i^2 - r_{\alpha i} r_{\beta i}) \right) \omega_\beta$$

$$= \sum_\beta I_{\alpha\beta} \omega_\beta \quad \text{or } \underline{L} = \underline{I} \cdot \underline{\omega} \quad ; \quad \underline{L} \text{ not } \parallel \text{ to } \underline{\omega}$$

$$T = \sum_i \frac{1}{2} m_i \left(\underline{\omega}^2 r_i^2 - \sum_\alpha \omega_\alpha r_{\alpha i} \sum_\beta \omega_\beta r_{\beta i} \right)$$

$$= \frac{1}{2} \sum_{\alpha, \beta} \left(\sum_i m_i (\delta_{\alpha\beta} r_i^2 - r_{\alpha i} r_{\beta i}) \right) \omega_\alpha \omega_\beta$$

$$= \frac{1}{2} \sum_{\alpha, \beta} I_{\alpha\beta} \omega_\alpha \omega_\beta = \frac{1}{2} \underline{\omega} \cdot \underline{I} \cdot \underline{\omega}$$

$\underline{I} = (I_{\alpha\beta}) =$ "moment of inertia tensor"

Then Lagrangian $L = T - V$, $V = \text{fun of } \{r_i\}$

& the torque eq is $\frac{d\underline{L}}{dt} = \underline{\Gamma}$

so \underline{I} controls the motion of the rigid body.

In detail, $\frac{d}{dt} (\underline{I}(t) \cdot \underline{\omega}(t)) = \underline{\Gamma}(t)$

$$\text{or } \underline{I} \cdot \dot{\underline{\omega}} + \dot{\underline{I}} \cdot \underline{\omega} = \underline{\Gamma}$$

$\swarrow \quad \nearrow$
 unknown t -dependence - see later

Computing \bar{I} :

trivial for discrete mass points $\{ (x_i, y_i, z_i); i=1, 2, \dots, N \}$

$$\bar{I}_{\alpha\beta} = \sum_i m_i (r_i^2 \delta_{\alpha\beta} - r_{i\alpha} r_{i\beta})$$

$$\Rightarrow \bar{I}_{xx} = \sum_i m_i (y_i^2 + z_i^2)$$

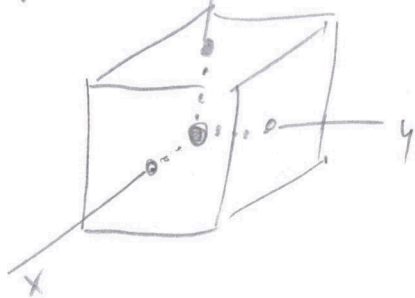
$$\bar{I}_{xy} = \sum_i m_i (-x_i y_i) \quad \text{etc.}$$

for continuous distributions (solid) use

$$\bar{I}_{\alpha\beta} = \int d^3r \rho(\underline{r}) \left(r^2 \delta_{\alpha\beta} - r_\alpha r_\beta \right)$$

↑
density

Example - uniform cube of side a , about CM



$$M = \rho a^3$$

$$\bar{I}_{xx} = \int_{\text{cube}} \rho d^3r (y^2 + z^2)$$

$$\bar{I}_{xy} = \int_{\text{cube}} \rho d^3r (-xy)$$

Other $\bar{I}_{\alpha\beta}$ are the same; $\bar{I}_{yy} = \bar{I}_{zz} = \bar{I}_{xx}$

$$\bar{I}_{yz} = \bar{I}_{zx} = \bar{I}_{xy}$$

$$\begin{aligned} \bar{I}_{xx} &= \rho \int_{-a/2}^{+a/2} dx \int_{-a/2}^{+a/2} dy \int_{-a/2}^{+a/2} dz (y^2 + z^2) \\ &= 2 \cdot \rho \cdot \frac{a}{2} \cdot 2 \cdot \frac{1}{3} \left(\frac{a}{2} \right)^3 = \rho a^5 / 6 = Ma^2 / 6 \end{aligned}$$

$$I_{xy} = -\rho \int_{-a/2}^{a/2} dx dy dz xy = -\rho \cdot 0 \cdot 0 \cdot a = 0$$

$$\text{so } \underline{I} = \begin{pmatrix} Ma^2/6 & 0 & 0 \\ 0 & Ma^2/6 & 0 \\ 0 & 0 & Ma^2/6 \end{pmatrix} \quad \text{and } \underline{L} = \frac{Ma^2}{6} \underline{\omega}$$

What about \underline{I} about a corner?

→ Parallel-axis theorem:

$$\text{start from } I_{CM, AB} = \int \rho d^3r (\underline{r}^2 \delta_{AB} - r_A r_B)$$

\underline{r} = vector from CM to point \underline{r} in body

for any other point P

$$I'_{AB} = \int \rho d^3r' (\underline{r}'^2 \delta_{AB} - r'_A r'_B)$$

\underline{r}' = vector from P to point \underline{r}' in body

$$\underline{r}' = \underline{r} - \underline{\Delta} \quad \underline{\Delta} = \text{vector from CM to P}$$

$$\text{so } I'_{AB} = \int \rho d^3r \left[(\underline{r} - \underline{\Delta})^2 \delta_{AB} - (\underline{r} - \underline{\Delta})_A (\underline{r} - \underline{\Delta})_B \right]$$

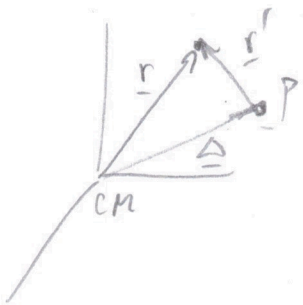
$$= \int \rho d^3r \left[\underline{r}^2 \delta_{AB} - r_A r_B \right. \rightarrow 0$$

$$\left. - 2 \underline{r} \cdot \underline{\Delta} \delta_{AB} + r_A \Delta_B + r_B \Delta_A \right.$$

$$\left. + \underline{\Delta}^2 \delta_{AB} - \Delta_A \Delta_B \right]$$

$\int d^3r r_A = 0$: def of CM

$$= I_{CM, AB} + M (\underline{\Delta}^2 \delta_{AB} - \Delta_A \Delta_B)$$



for the cube: $\underline{\Delta}$ = vector from CM to corner

$$= \left(\frac{a}{2}, \frac{a}{2}, \frac{a}{2} \right) \text{ say}$$

$$\text{so } I'_{xx} = I_{xx} + M \left(3 \cdot \left| \frac{a}{2} \right|^2 - \frac{a}{2} \cdot \frac{a}{2} \right) \\ = \frac{1}{6} Ma^2 + \frac{Ma^2}{2} = \frac{2}{3} Ma^2$$

$$I'_{xy} = I_{xy} + M \left(0 - \frac{a}{2} \cdot \frac{a}{2} \right) = -Ma^2/4$$

ok. - same symmetry because all 3 Δ 's are same

$$\rightarrow \underline{I} = \begin{pmatrix} I_0 & I_1 & I_1 \\ & I_0 & I_1 \\ \text{sym} & & I_0 \end{pmatrix} \quad I_0 = \frac{2}{3} Ma^2, I_1 = -\frac{1}{4} Ma^2$$

Effect on \underline{L} :

$$\underline{\omega} = (\omega, 0, 0) \text{ about CM: } \underline{L}_{\text{cm}} = \underline{I}_{\text{cm}} \cdot \underline{\omega} \\ = \left(\frac{Ma^2}{6} \omega, 0, 0 \right) \\ = \frac{Ma^2}{6} \underline{\omega}$$

$$\text{about corner } \underline{L}' = \underline{I}' \cdot \underline{\omega} = (I_0 \omega, I_1 \omega, I_1 \omega) \\ \text{not } \parallel \text{ to } \underline{\omega}$$

$$\omega = (1, 1, 1) \quad \underline{L}_{\text{cm}} = \frac{Ma^2}{6} \underline{\omega} \text{ again}$$

$$\underline{L}' = (I_0 + 2I_1) \underline{\omega} = \frac{Ma^2}{6} \underline{\omega} \text{ again!}$$

\rightarrow Highly symmetric, same as a sphere.